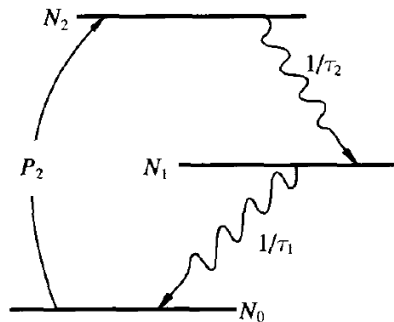


Laser Physics I (PHYS/ECE 464), Fall 2022
Homework #8, Due Monday Nov. 7

1.

In the diagram shown below, the pump P_2 (i.e., electrons, flash lamp, another laser, etc.) excites atoms from state 0 to state 2, nothing to state 1. To make the problem simple and tractable, assume state 0 is not depleted to any significant extent for any time (i.e., $dN_0/dt = 0$); use the simple decay route indicated; neglect stimulated emission; assume $\tau_2 = 1 \mu\text{s}$ and $\tau_1 = 2 \mu\text{s}$; and let $P_2 = 10^{20} \text{ cm}^{-3} \text{ s}^{-1}$. Use symbols for (a) and (b) and find numerical values for (c) and (d).



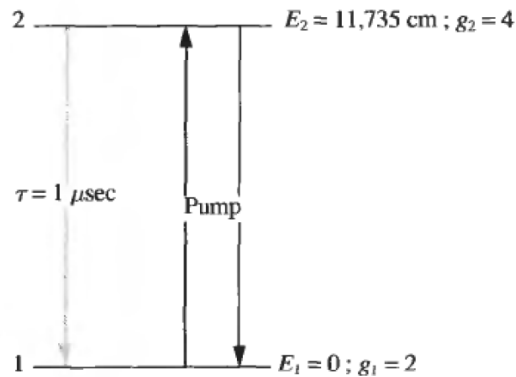
- (a) What are the rate equations for states 2 and 1?
- (b) Give an expression for the densities $N_{2,1}$ as a function of time.
- (c) Over what time interval, δt , is the population difference $N_2 - N_1 > 0$?
- (d) What are the steady-state populations in 2 and 1?

2.

Consider the atomic system shown below being irradiated by an external wave tuned to the center of the $2 \rightarrow 1$ transition with 1 being the ground state. The wave pumps the atoms from 1 to 2 and also stimulates the atoms back to 1 from 2. In addition, the atoms in state 2 decay back to 1 by spontaneous emission and/or by other processes with a rate given by $(\tau)^{-1}$. The total density of atoms is $[N]$. Assume $\sigma = 10^{-14} \text{ cm}^2$

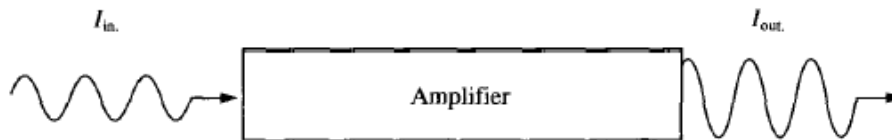
- (a) Formulate the rate equations for the two states in terms of the intensity of the external wave, the stimulated emission cross section, the frequency $h\nu = E_2 - E_1$, τ , and the degeneracies of the states (g_2, g_1).

- (b) What would be the population ratio N_2/N_1 if the intensity of the external wave were infinite?
- (c) What must be the intensity to make the population ratio N_2/N_1 equal to 1/2?
- (d) If the ambient temperature were such that $kT = 208 \text{ cm}^{-1}$ and the intensity were zero, what is the steady state population ratio N_2/N_1 ?



3.

An experiment involving a homogeneously broadened optical amplifier is depicted in the diagram below. For an input intensity of 1 W/cm^2 , the gain (output/input) is 10 dB. If the input intensity is doubled to 2 W/cm^2 , the gain is reduced to 9 dB.



- (a) What is the small-signal gain (i.e., $I_{in} \rightarrow 0$) of this amplifier (in dB)?
- (b) What is the saturation intensity?
- (c) What is the maximum power (per unit area) that can be extracted from this amplifier (in limit of large input intensity)?
- (d) What must be the input intensity to extract 50% of this maximum?

Note: $\text{dB (gain)} = 10 \log_{10}(P_{out}/P_{in})$ or $10 \log_{10}(I_{out}/I_{in})$

1.

(a) $\frac{dN_2}{dt} = \frac{\sigma I_p}{h\nu} \left[\frac{g_2}{g_1} N_1 - N_2 \right] - \frac{N_2}{\tau}$; There is no need to write a separate equation for N_1

since atoms must be conserved and thus $N_1 + N_2 = [N]$;

(b) If $I_p \rightarrow \infty$, then the bracket in the above must be zero to prevent an infinity appearing in a physical equation. Thus $N_2/N_1 = g_2/g_1$.

(c) For a steady-state situation: $N_2 \left[1 + \frac{\sigma \tau}{h\nu} I_p \right] = \frac{g_2 \sigma \tau}{g_1 h\nu} I_p N_1$ or $\frac{N_2}{N_1} = \frac{(g_2/g_1) \cdot (I_p/I_s)}{1 + (I_p/I_s)}$

where $I_s = \frac{h\nu}{\sigma \tau}$; This ratio equals 0.5 when $I_p/I_s = 0.25$ for $g_2/g_1=2$; $I_s = 23.3 \text{ W/cm}^2$;

Thus $I = 5.82 \text{ W/cm}^2$; (d) $N_2/N_1 = (g_2/g_1) \exp[-E/kT] = 6.25 \times 10^{-25}$; safe to ignore N_2 .

2.

This is a reasonable model for the pulsed N_2 laser which has a very high gain and lases at $0.337 \mu\text{m}$. Its major drawback is that it is self-terminating because the inversion can not be maintained indefinitely – fact that comes out of the analysis that follows.

$\frac{dN_2}{dt} = P_2 - \frac{N_2}{\tau_2}$ whose solution is: $N_2(t) = P_2 \tau_2 (1 - \exp[-t/\tau_2])$

$\frac{dN_1}{dt} = + \frac{N_2}{\tau_2} - \frac{N_1}{\tau_1}$ or $\frac{dN_1}{dt} + \frac{N_1}{\tau_1} = P_2 (1 - \exp[-t/\tau_2])$

$N_1 = P_2 \tau_1 \left\{ 1 - \frac{\tau_1/\tau_2}{\tau_1/\tau_2 - 1} e^{-t/\tau_1} + \frac{1}{\tau_1/\tau_2 - 1} e^{-t/\tau_2} \right\}$

It is informative to consider the steady-state populations, i.e., where $t \gg \tau_{2,1}$. $N_2(t \rightarrow \infty) = P_2 \tau_2$ and $N_1(t \rightarrow \infty) = P_2 \tau_1$. Note that since $\tau_1 > \tau_2$, we have the undesirable situation of $N_1 > N_2$ which means that the system will not lase in a steady state. However, one can obtain a transient inversion (and a laser) as the sketch below indicates.

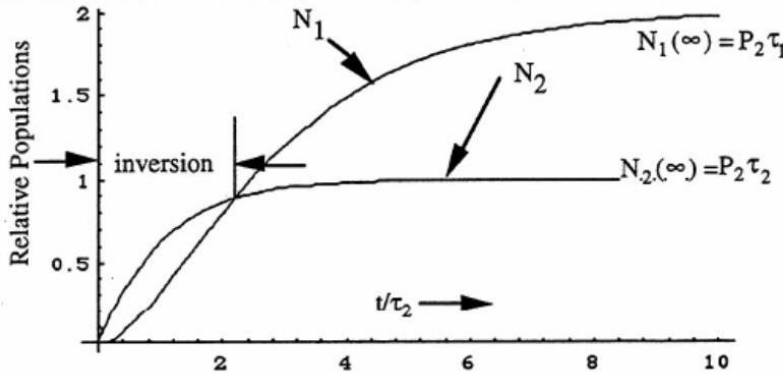


Figure for problem 7.10

$N_2(t \rightarrow \infty) = 10^{20} \times 10^{-6} = 10^{14} \text{ cm}^{-3}$, $N_1(t \rightarrow \infty) = 10^{20} \times 2 \times 10^{-6} = 2 \times 10^{14} \text{ cm}^{-3}$

Let $t/\tau_1 = x$; $(\tau_1/\tau_2) = 2$; $N_1 = N_2$ when $2(1 - 2e^{-x} + e^{-2x}) = (1 - e^{-2x})$;

Collect terms, multiply by e^{2x} and factor: $f(x) = [e^x - 3][e^x - 1] = 0$;

where $x = t/\tau_1$; $F(x) = 0$ at $x = 0$ (i.e. at the start) or $x = t/\tau_1 = \ln 3$; $\therefore t = 1.0986 \tau_1 = 2.2 \mu\text{sec}$

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$$I_{out} = 10 \frac{G_{dB}}{10} I_{in} \rightarrow \begin{cases} \text{for } G=10 \text{ dB} \rightarrow \frac{I_{out}}{I_{in}} = 10 = G_1 \\ \text{for } G=9 \text{ dB} \rightarrow \frac{I_{out}}{I_{in}} = 10^{0.9} \approx 7.9 = G_2 \end{cases}$$

$$\ln G + \tilde{g}(v) \frac{I_{in}}{I_s} (G-1) = \alpha_0 l_g ; \quad \tilde{g}(v) = 1$$

$$\begin{cases} \ln G_1 + \frac{I_{in}}{I_s} (G_1 - 1) = \alpha_0 l_g & \left\{ \begin{array}{l} \ln 10 + \frac{1}{I_s} (10-1) = \alpha_0 l_g \\ \ln 7.9 + \frac{2}{I_s} (7.9-1) = \alpha_0 l_g \end{array} \right. \end{cases}$$

$$\rightarrow \begin{cases} 2.3 + \frac{9}{I_s} = \alpha_0 l_g \\ 2.06 + \frac{13.8}{I_s} = \alpha_0 l_g \end{cases} \rightarrow \begin{cases} \alpha_0 l_g = 2.75 \\ I_s = 20 \left[\frac{W}{cm^2} \right] \quad (b) \end{cases}$$

$$\rightarrow G_0 = \exp(\alpha_0 l_g) = 15.64 = 11.94 \text{ dB} \quad (a)$$

$$(c) \frac{DP}{\text{area} \cdot \text{length}} = -\frac{\alpha_0(v) I_s}{\tilde{g}(v)} \rightarrow \frac{DP}{\text{area}} = l_g \alpha_0(v) I_s = (2.75) \cdot 20 = 55 \left[\frac{W}{cm^2} \right]$$

$$(d) \begin{cases} I_{out} = I_{in} + \left[\frac{\alpha_0(v) I_s l_g}{\tilde{g}(v)} \right] \rightarrow I_{out} - I_{in} = \frac{1}{2} \times 55 = 27.5 \\ I_{out} = \frac{1}{2} I_{in} \end{cases}$$

$$\rightarrow \ln G + \frac{I_{in}}{I_s} (G-1) = \alpha_0(v) l_g \rightarrow \ln \frac{I_{out}}{I_{in}} + \frac{I_{in}}{I_s} \left(\frac{I_{out}}{I_{in}} - 1 \right) = \alpha_0 l_g$$

$$\rightarrow \ln \frac{I_{out}}{I_{in}} + \frac{I_{in}}{20} \left(\frac{I_{out} - I_{in}}{I_{in}} \right) = 2.75 \rightarrow$$

$$\ln \frac{I_{out}}{I_{in}} + \frac{27.5}{20} = 2.75 \rightarrow \begin{cases} \frac{I_{out}}{I_{in}} = 3.93 \rightarrow I_{in} = 9.38 \\ I_{out} - I_{in} = 27.5 \quad \left[\frac{W}{cm^2} \right] \end{cases}$$

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